
Fluctuation-Dissipation Dynamics of Fission and Heavy-Ion Fusion Reactions

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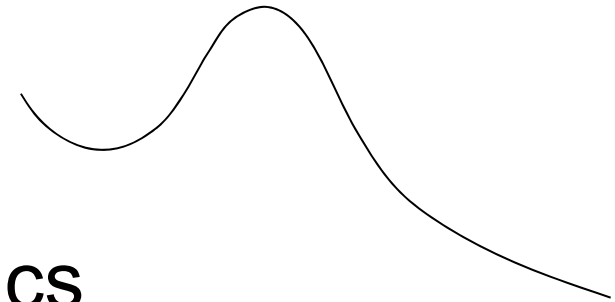
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INT13-3 Quantitative Large Amplitude Shape Dynamics:
fission and heavy ion fusion

Seattle, WA, 15 Oct., 2013

Theories for fission

- Transition state method
 - Statistical approach
 - Fission width
- Fluctuation-dissipation dynamics
 - Dynamical approach (Macroscopic)
 - Fission width
 - Saddle-to-scission dynamics
- Time-dependent mean field theory
 - Dynamical approach (Microscopic)
 - Saddle-to-scission dynamics



Transition state method

- Fission width

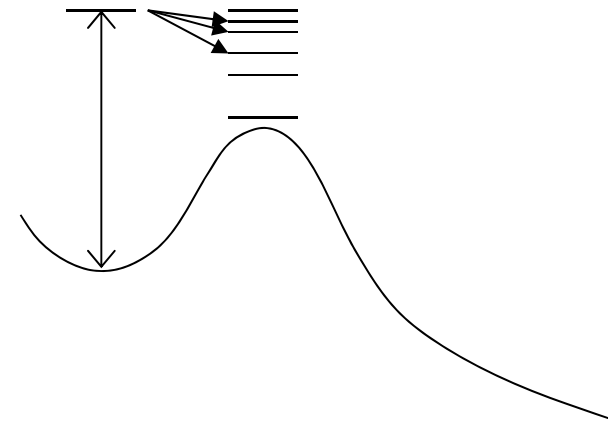
$$dE \int_0^{E-B_f} \frac{v dp}{2\pi\hbar} \rho_A^*(E - B_f - \varepsilon) = dE \frac{\Gamma_f}{\hbar} \rho_A(E) \quad \# \text{ of decay per unit time}$$

$$\Gamma_f = \frac{1}{2\pi\rho_A(E)} \int_0^{E-B_f} d\varepsilon \rho_A^*(E - B_f - \varepsilon)$$

- Fermi gas level density

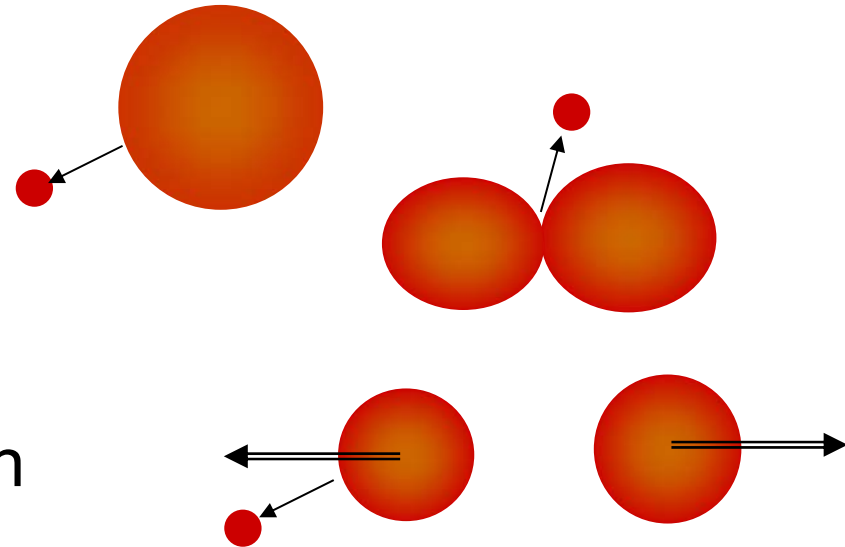
$$\rho(E^*) \propto \exp\left(2\sqrt{aE^*}\right)$$

$$\Gamma_f = \frac{T}{2\pi} \exp\left(-\frac{B_f}{T}\right) \quad E^* = aT^2$$



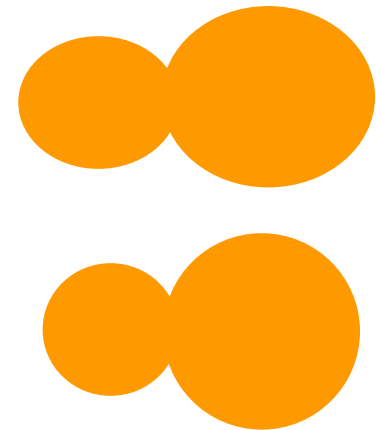
Key quantities in fission

- Fission rate
 - Height of fission barrier
- Particle emission
 - Neutron emission
 - Pre-scission neutrons
 - Scission neutrons
 - Post-scission neutrons
 - Charged particle emission
 - Gamma emission
- Fission fragments
 - Mass distribution
 - Total kinetic energy distribution



Mass & TKE distribution

- Mass distribution is essentially determined by shell correction energy
 - At saddle :position & height fission barrier
 - Fission valleys and ridges
 - Fragments :magic number
- TKE (total kinetic energy)
 - Mainly Coulomb repulsion
 - Scission configuration
 - Nature of nuclear dissipation
- Dynamical treatment is necessary



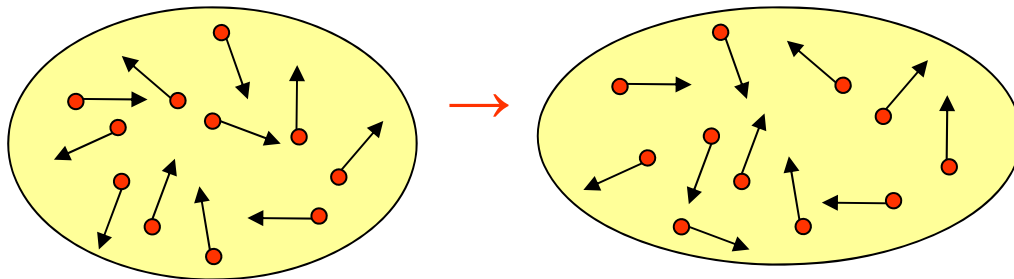
Fluctuation-dissipation dynamics

- Brownian picture

- Macroscopic degree(s) of freedom interacting with microscopic degrees of freedom in thermal motion

Dissipation (collective \rightarrow nucleonic) \Leftarrow Friction

Fluctuation (nucleonic \rightarrow collective) \Leftarrow Random force



- Macroscopic degrees of freedom

= Nuclear shape

(elongation, deformation, neck, mass asymmetry etc.)

Two approaches

Langevin equation

$$\frac{dq}{dt} = \frac{p}{m} \quad \frac{dp}{dt} = -\frac{\partial U}{\partial q} - \frac{\gamma}{m} p + \sqrt{\gamma T} R(t)$$

$$\langle R(t) \rangle = 0, \quad \langle R(t_1)R(t_2) \rangle = 2\delta(t_1 - t_2)$$

Eq. of motion of a Brownian particle

Focker-Planck (Kramers) equation

$$\frac{\partial f}{\partial t} = -\frac{p}{m} \frac{\partial f}{\partial q} + \frac{\partial U}{\partial q} \frac{\partial f}{\partial p} + \frac{\gamma}{m} \frac{\partial}{\partial p} (pf) + \gamma T \frac{\partial^2 f}{\partial p^2}$$

Distribution of the Brownian particles

Fission width by Kramers theory

- Diffusion process over barrier

$$\frac{\partial f}{\partial t} = -\frac{p}{m} \frac{\partial f}{\partial q} + \frac{\partial U}{\partial q} \frac{\partial f}{\partial p} + \frac{\gamma}{m} \frac{\partial}{\partial p} (pf) + \gamma T \frac{\partial^2 f}{\partial p^2}$$

- $U =$ parabola + inverse parabola

- Analytic solution

$$\Gamma_f = K \frac{\hbar \omega}{2\pi} \exp\left(-\frac{B_f}{T}\right)$$

$$U = \begin{cases} \frac{1}{2} m \omega^2 q^2 \\ B_f - \frac{1}{2} m \omega_B^2 (q - q_B)^2 \end{cases}$$

$$K = \frac{1}{2\omega_B} \left[\sqrt{\beta^2 + 4\omega_B^2} - \beta \right], \quad \beta = \frac{\gamma}{m}$$

Kramers factor

cf. BW

$$\Gamma_f = \frac{T}{2\pi} \exp\left(-\frac{B_f}{T}\right)$$

Transport coefficients

- Inertia mass tensor

- Hydrodynamical mass

- Werner-Wheeler approximation

- Cranking mass

- Friction tensor

- One-body friction

- Wall and Window formula

- Interaction of nucleons with nuclear surface (wall)

- Exchanging nucleons through the neck window

- Two-body viscosity

- Energy loss by nucleon-nucleon collisions
-

TKE systematics

■ Viola systematics (1985, V. E. Viola)

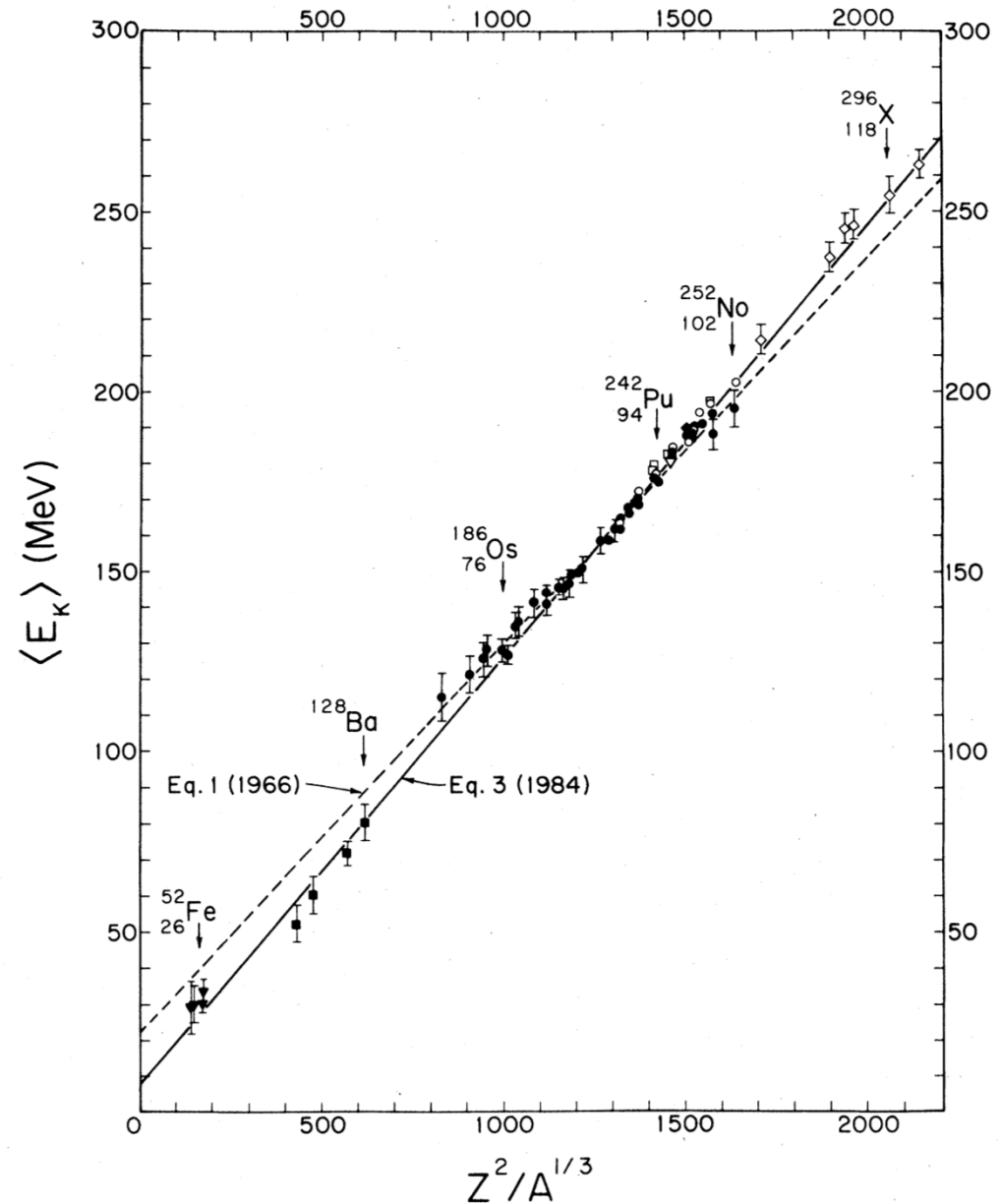
$$\langle E_K \rangle = 0.1071 Z^2 / A^{1/3} + 22.2 \text{ MeV}$$

Data before 1966

$$\langle E_K \rangle = 0.1189 Z^2 / A^{1/3} + 7.3 \text{ MeV.}$$

Data up to 1984

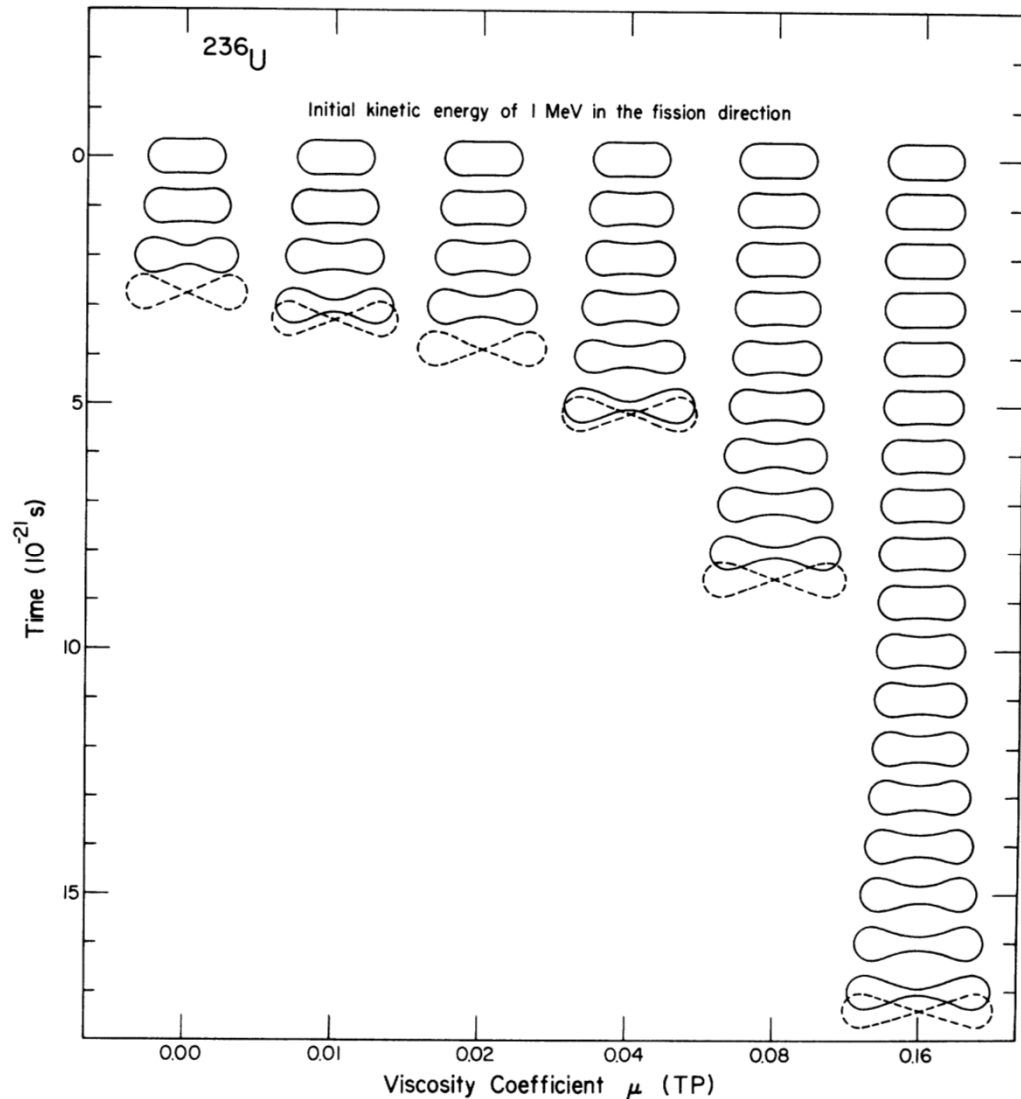
- Main contribution to TKE comes from Coulomb repulsion
- Measure of the fragment deformation



Saddle-to-scission dynamics

- Saddle-to-scission time (τ_{SSC}) depends on the dissipation
- Scission shape also depends on the dissipation
- Fragment TKE also depends on the dissipation

$$TKE = K_{pre} + V_C$$



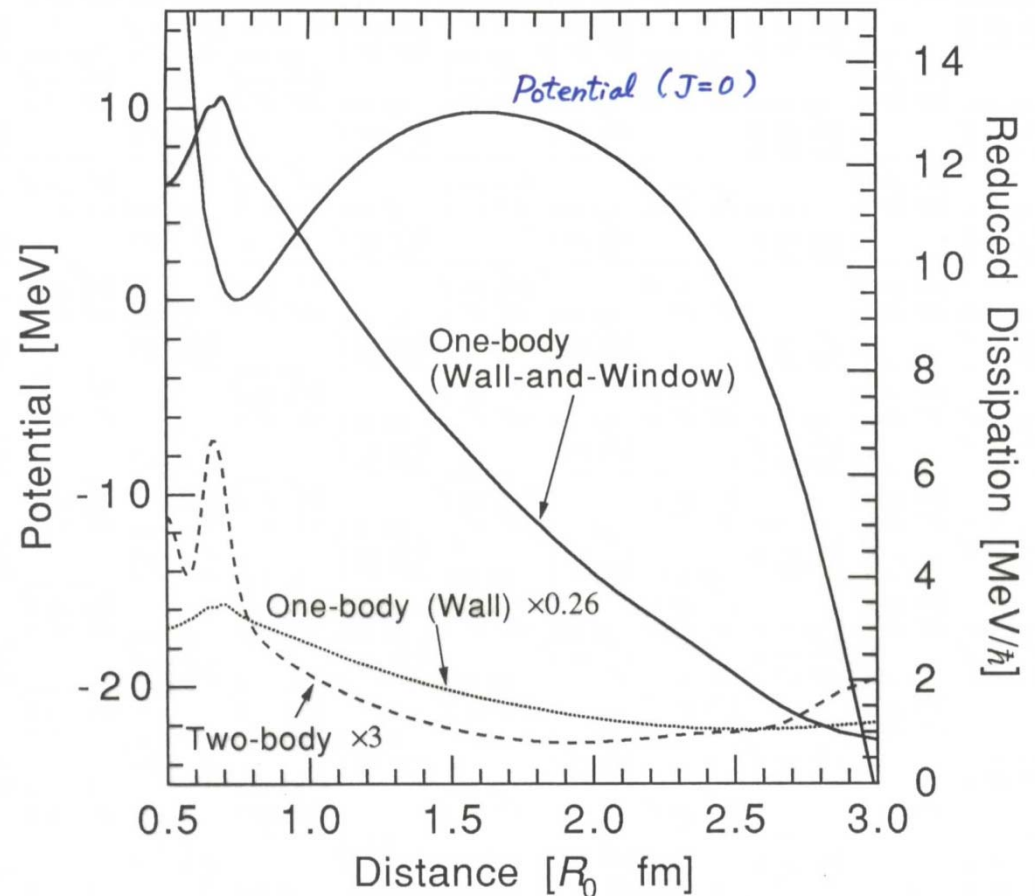
Coordinate dependence of friction

- Reduced dissipation

$$\beta = \gamma / m$$

- Different dependence on elongation

- Wall-and-Window
- Wall
- Two-body



Time-dependent fission rate

■ Delay of fission

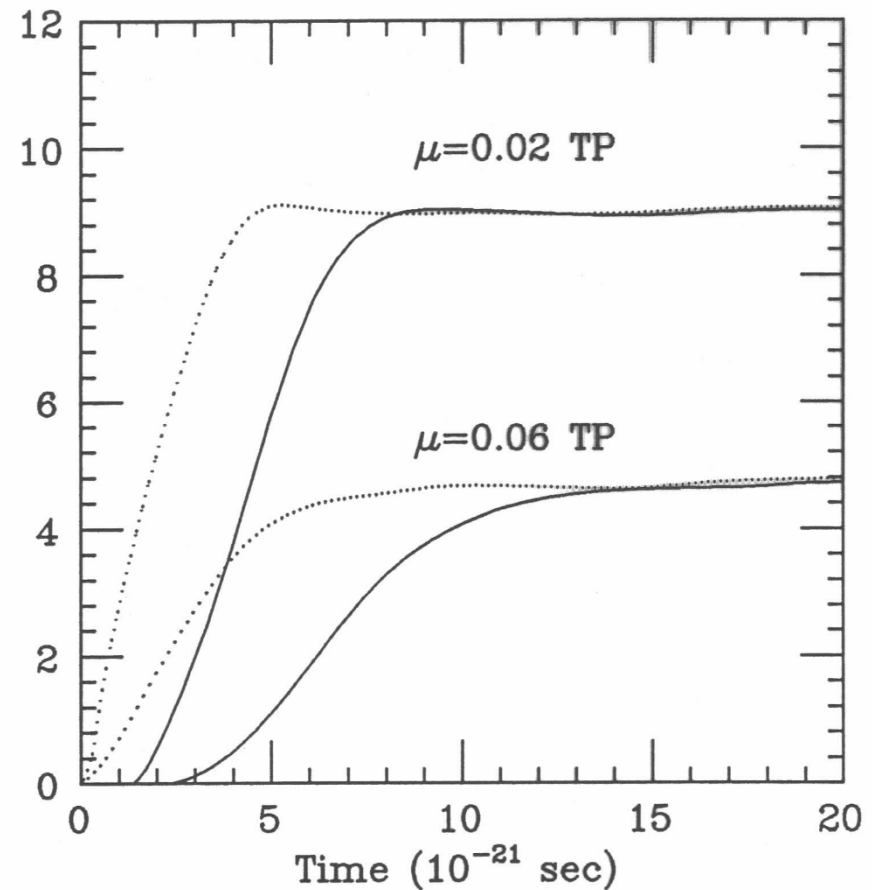
$$\tau_{delay} = \tau_{tr} + \tau_{ssc}$$

- Transient time
- Saddle-to-scission time

■ Typical time

- $\tau_{tr}, \tau_{ssc} \approx 10^{-21}$ s : two-body
- $\tau_{tr}, \tau_{ssc} \approx 10^{-20}$ s : one-body

Fission Rate ($10^{+18}/\text{sec}$)



Fission and nuclear dissipation

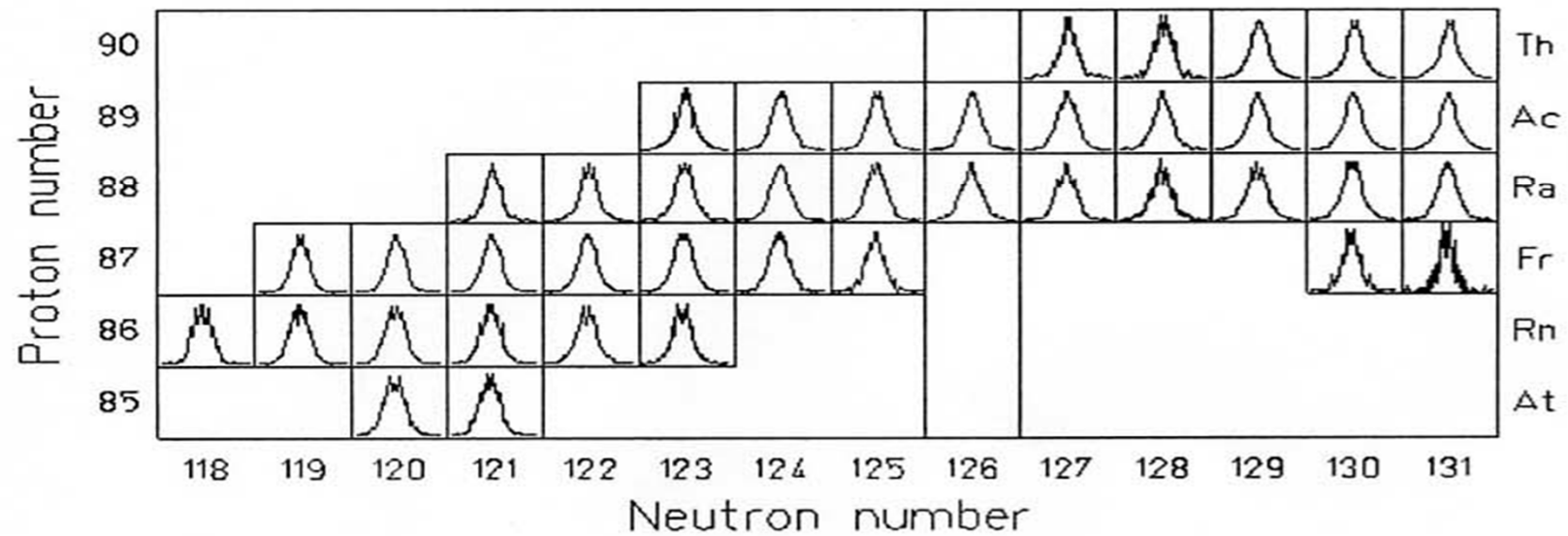
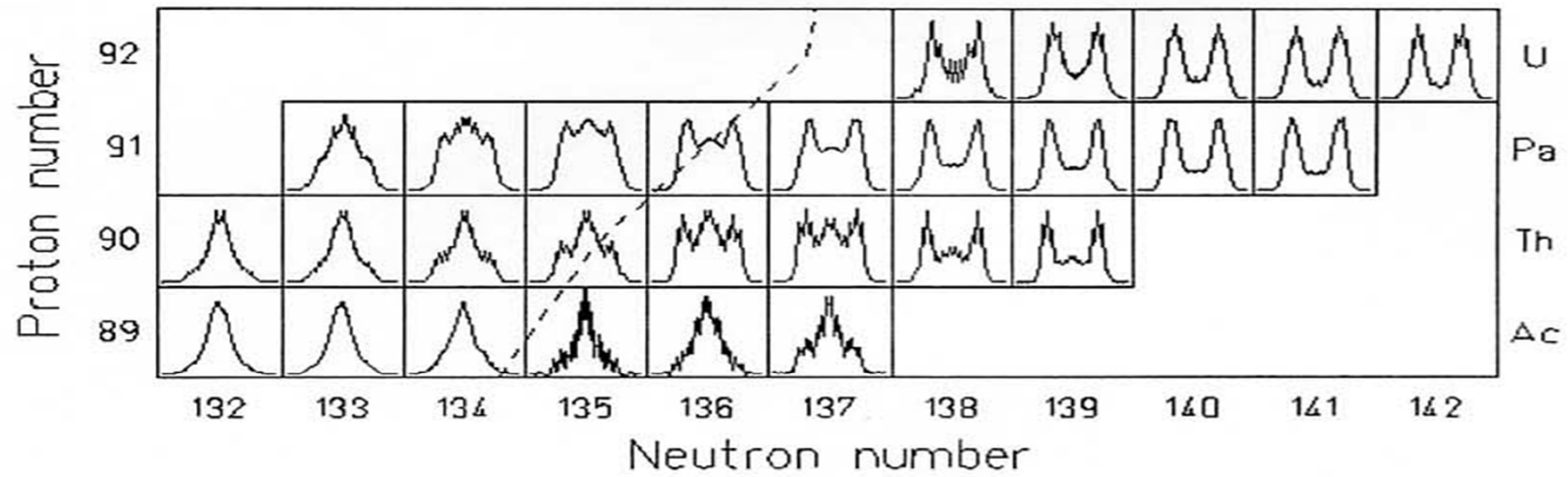
- Two types of dissipation tensors
 - One-body Wall-and-Window dissipation
 - Two-body hydrodynamical dissipation

$$\tau_{delay} = \tau_{tr} + \tau_{ssc}$$

$$TKE = K_{pre} + V_C$$

80.7MeV		σ_{fus}	σ_{fiss}	σ_{er}	v_{pre}	TKE
1-body		1150	790	360	2.93	135.1
2-body	0.02 TP	1150	928	222	2.06	124.9
	0.06 TP	1150	817	333	2.84	108.6
Exp.		1150	767	383	3.2 ± 0.3	–
195.8MeV		σ_{fus}	σ_{fiss}	σ_{er}	v_{pre}	TKE
1-body		1400	1244	156	7.33	137.0
2-body	0.02 TP	1400	1338	62	4.79	123.6
	0.06 TP	1400	1261	139	7.03	107.4
Exp.		1400	–	–	7.7 ± 0.3	139

Fission modes



K. -H. Schmidt et al.

Shell correction energy

- Strutinsky method

$$\Delta E_{shell} = \sum_i^N \varepsilon_i - \tilde{E}$$

$$N = \int^{\varepsilon_F} g(\varepsilon) d\varepsilon, \quad \tilde{E} = \int^{\varepsilon_F} g(\varepsilon) \varepsilon d\varepsilon$$

$$g(\varepsilon) = \sum_i^N \frac{1}{\sqrt{2\pi}\sigma} \exp\left(-\frac{(\varepsilon - \varepsilon_i)^2}{2\sigma^2}\right) \sum_m H_m\left(\frac{\varepsilon - \varepsilon_i}{\sigma}\right)$$

- Macro-microscopic approach

$$\tilde{E} \rightarrow E_{Macro}, \quad E = E_{Macro} + \Delta E_{shell}$$

- Damping of shell correction

$$\Delta E_{shell}(q, E_x) = \Delta E_{shell}(q, E_x = 0) \exp(-E_x / E_d)$$

- Essential for asymmetric fission

Extension to multi-dimension

Multi-dimensional Langevin equation

$$\begin{aligned}\frac{dq_i}{dt} &= (m^{-1})_{ij} p_j & i, j, k = 1, \dots, N \\ \frac{dp_i}{dt} &= -\frac{\partial V}{\partial q_i} - \frac{1}{2} \frac{\partial}{\partial q_i} (m^{-1})_{jk} p_j p_k - \gamma_{ij} (m^{-1})_{jk} p_k + g_{ij} R_j(t) \\ \langle R_i(t) \rangle &= 0, \quad \langle R_i(t_1) R_j(t_2) \rangle = 2\delta_{ij} \delta(t_1 - t_2) & \sum_k g_{ik} g_{jk} = T\gamma_{ij}\end{aligned}$$

- $m_{ij}(q)$ Hydrodynamical inertial mass
- $\gamma_{ij}(q)$ Wall-and-Window (one-body) friction
- $V(q)$ Macro-microscopic potential

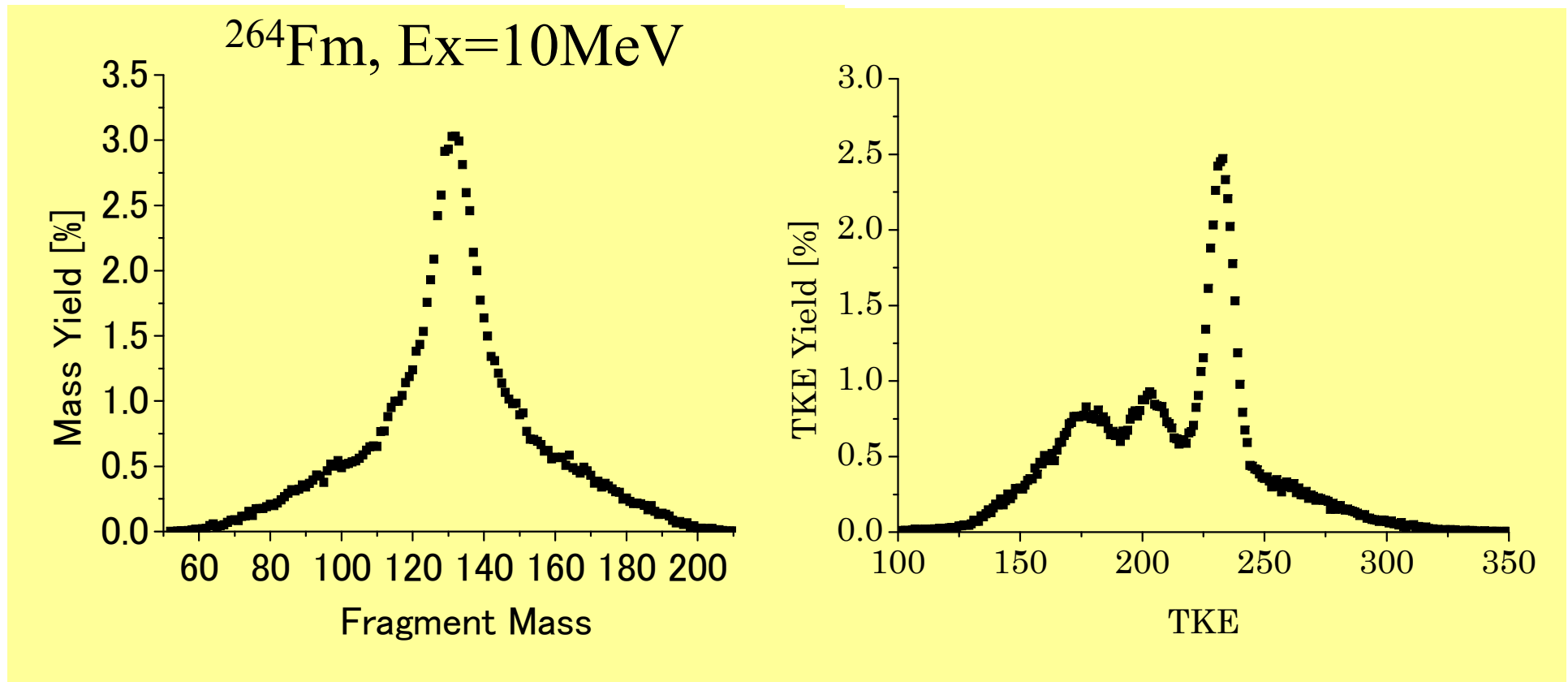
$\{q_i\}$: collective parameters

(elongation, fragment deformation, neck parameter, mass asymmetry)

TKE and mass distribution of fragments

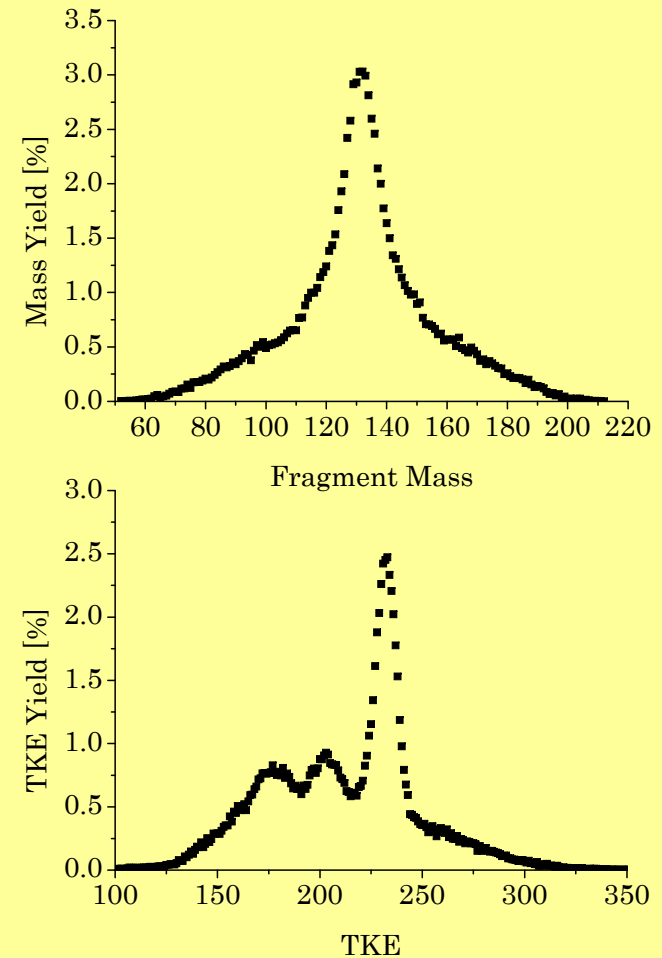
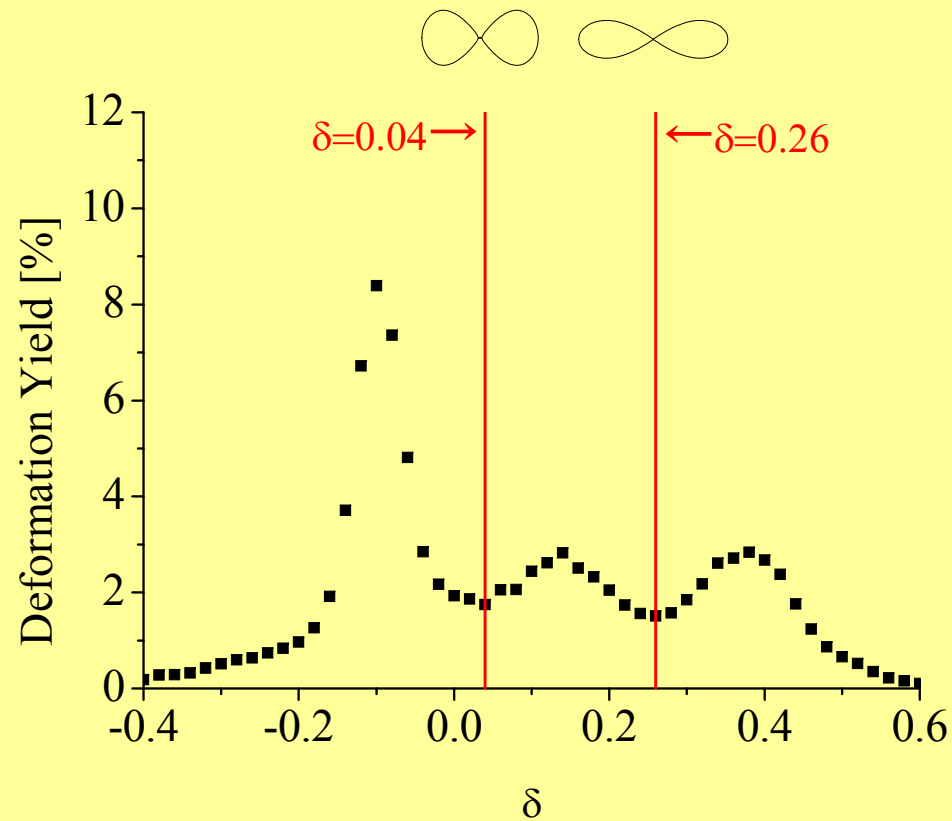
Three-dimensional Langevin calculation

elongation, fragment deformation, mass-asymmetry



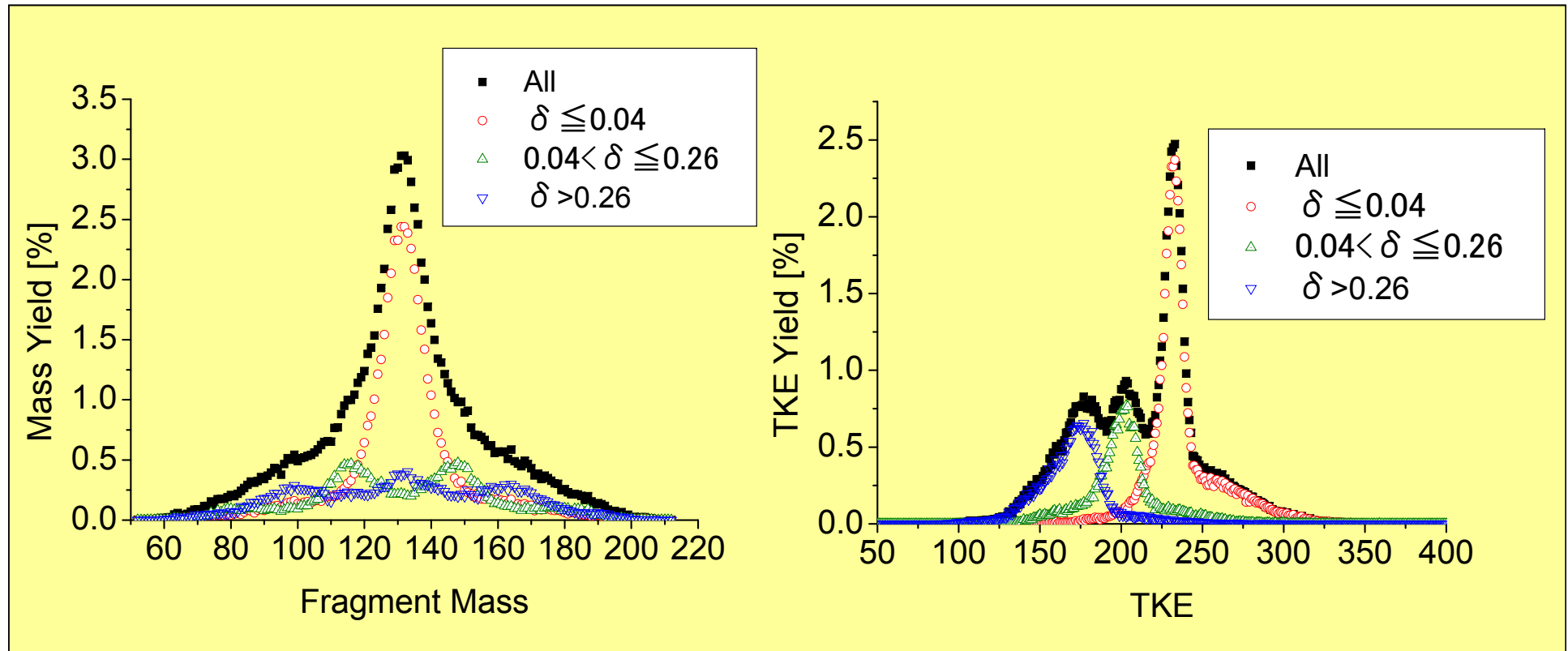
Numbers of the peaks are different in mass and TKE

Deformation of the fragments at scission



Fission modes

T. Asano et al, (J. Nucl. Radiochem. Sci. 5 (2004) 1)

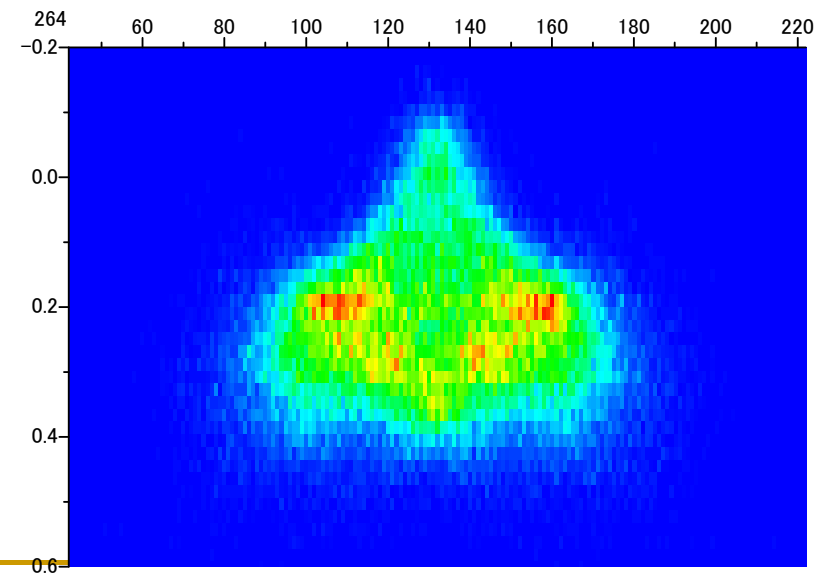
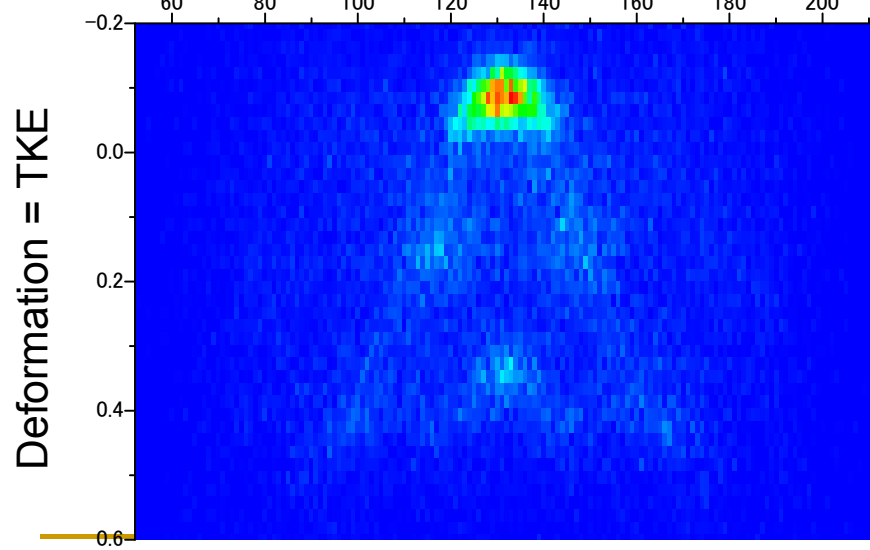
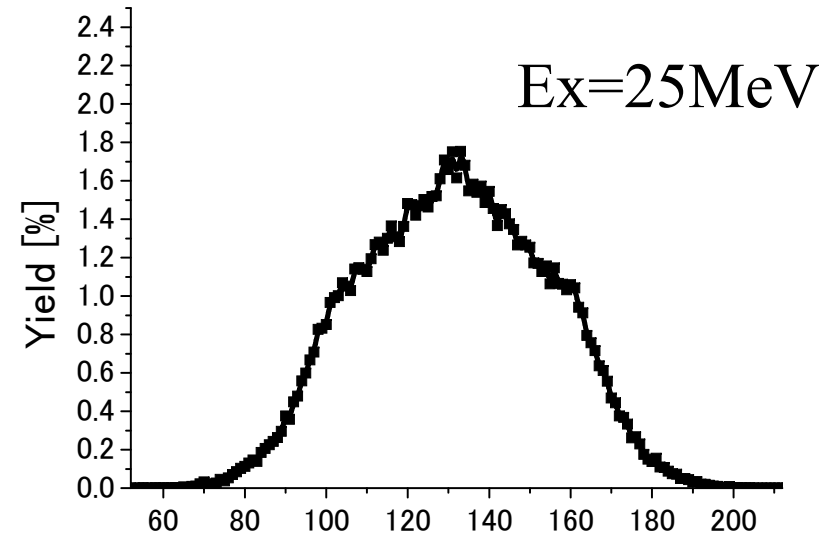
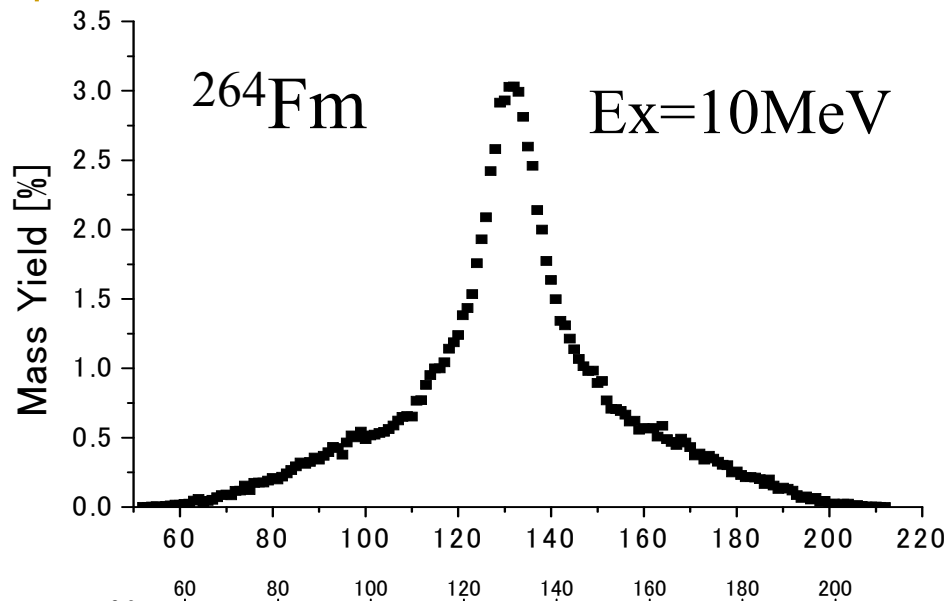


$\delta \leq 0.04$: Mass-symmetric & High TKE mode

$0.04 < \delta \leq 0.26$: Mass-asymmetric & Medium TKE mode

$\delta > 0.26$: Mass-symmetric ? & Low TKE mode

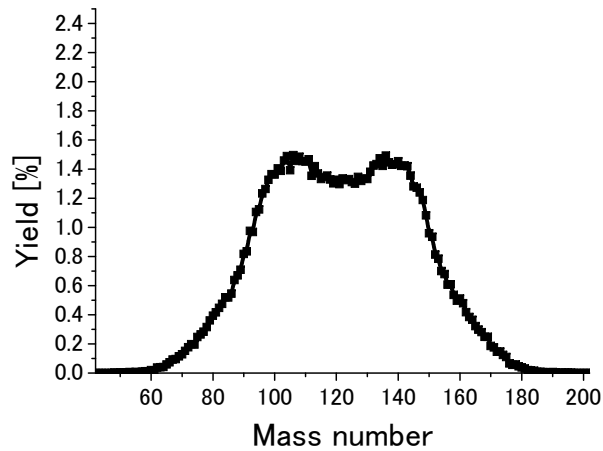
Energy dependence of mass distribution



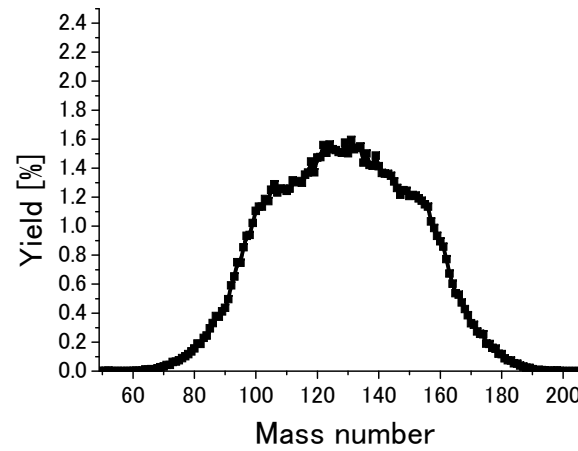
Isotopic dependence of mass distribution

Ex=25MeV

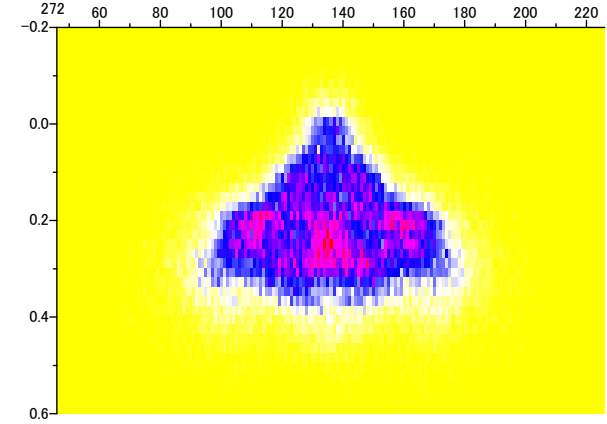
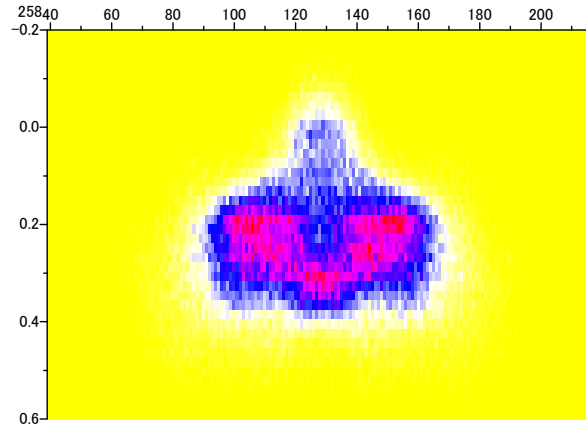
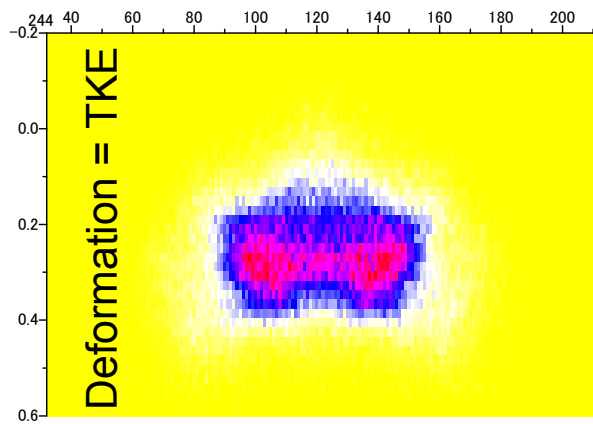
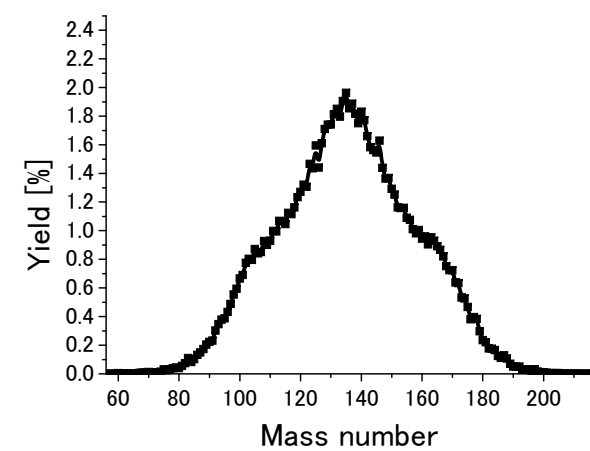
^{244}Fm



^{258}Fm



^{272}Fm

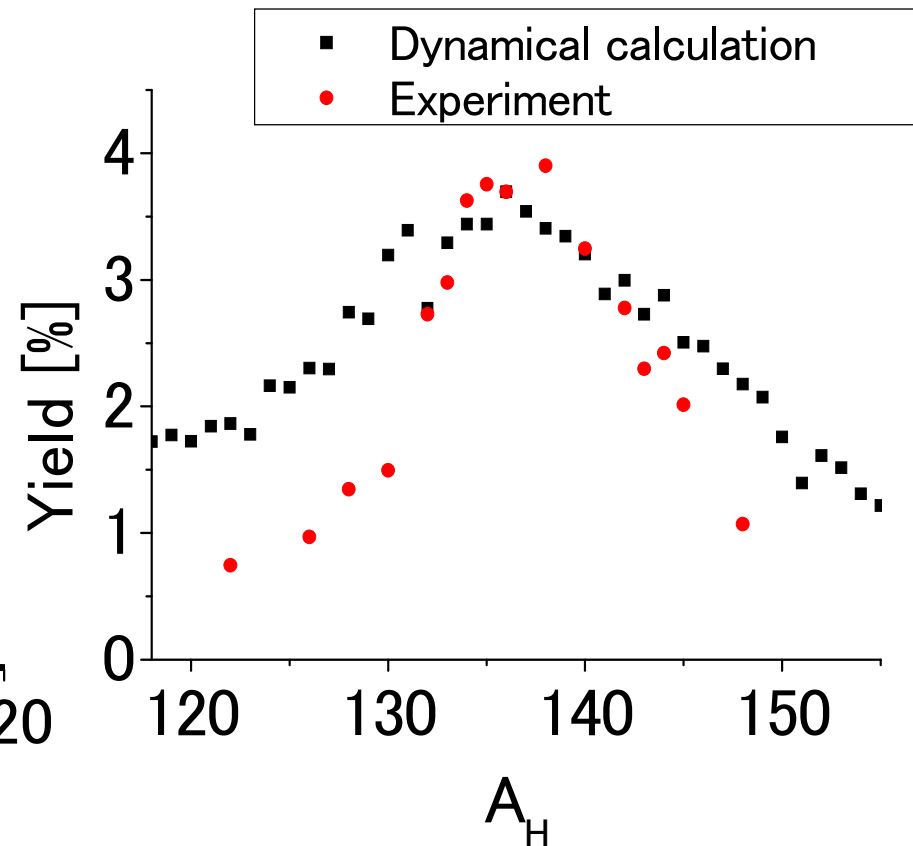
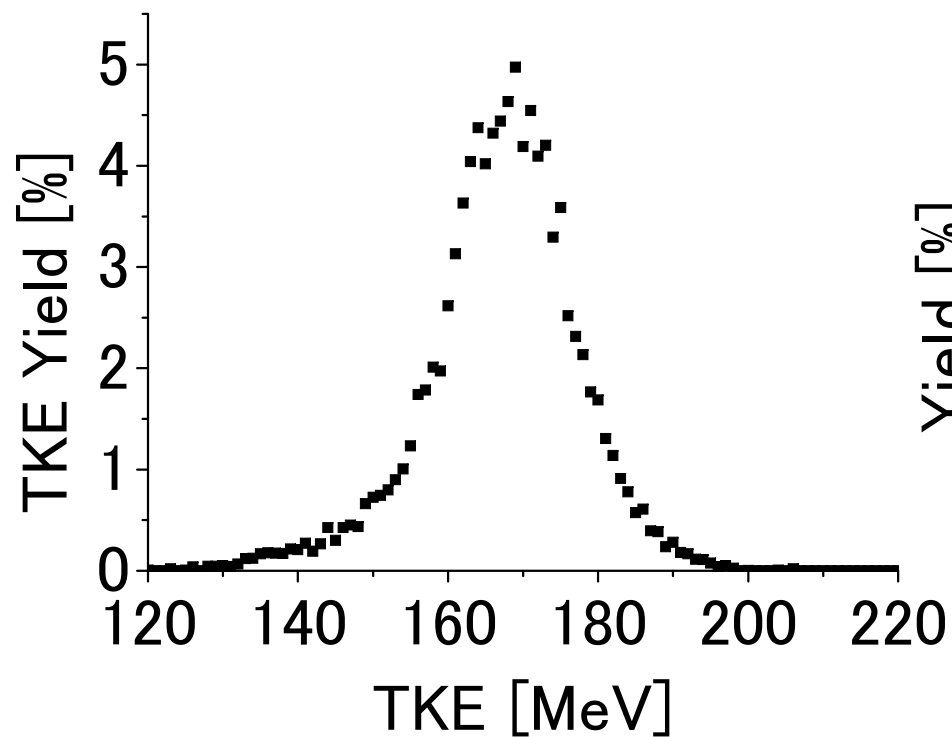


TKE and mass distribution of fragments

Three-dimensional Langevin calculation

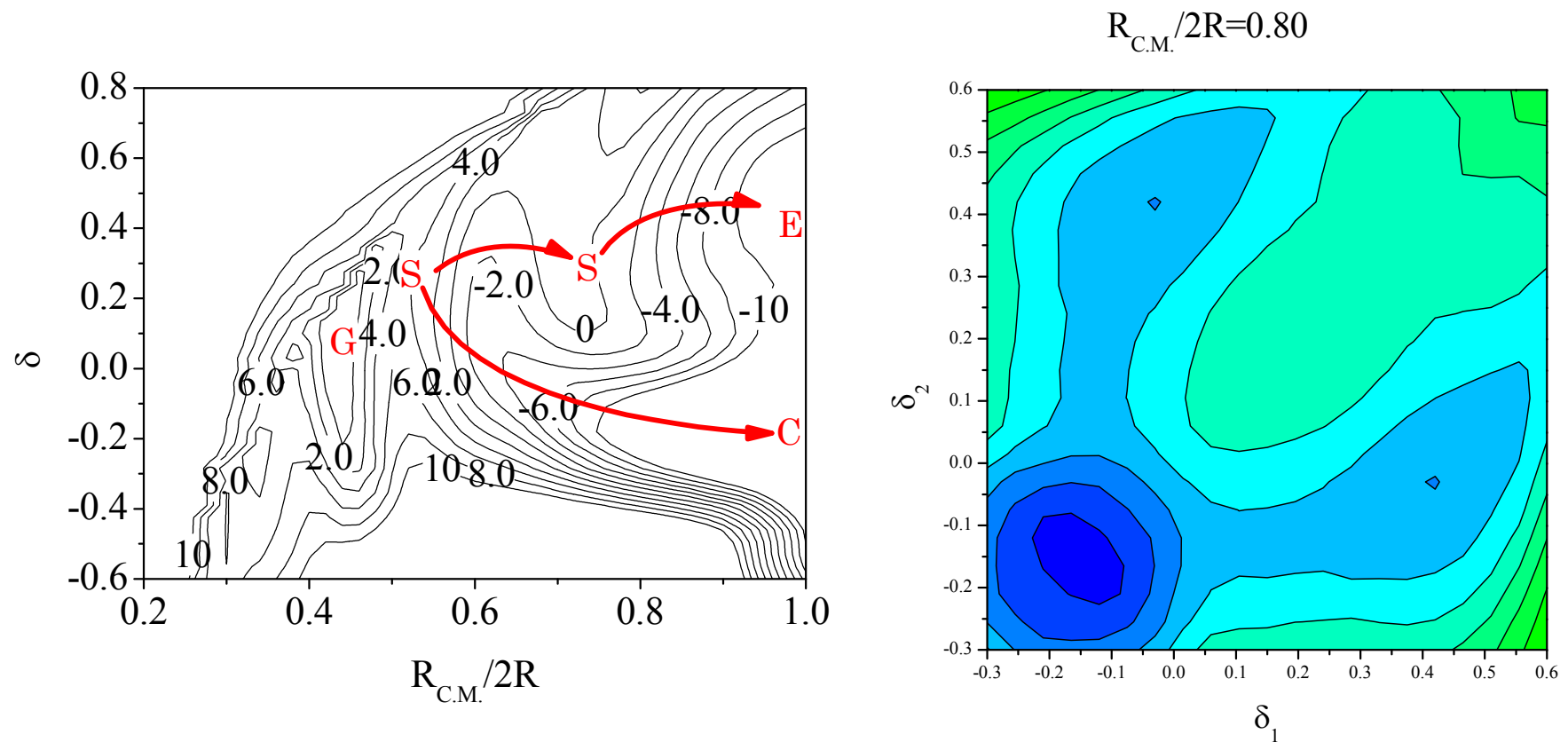
elongation, fragment deformation, mass-asymmetry

^{236}U , $E_x=20\text{MeV}$



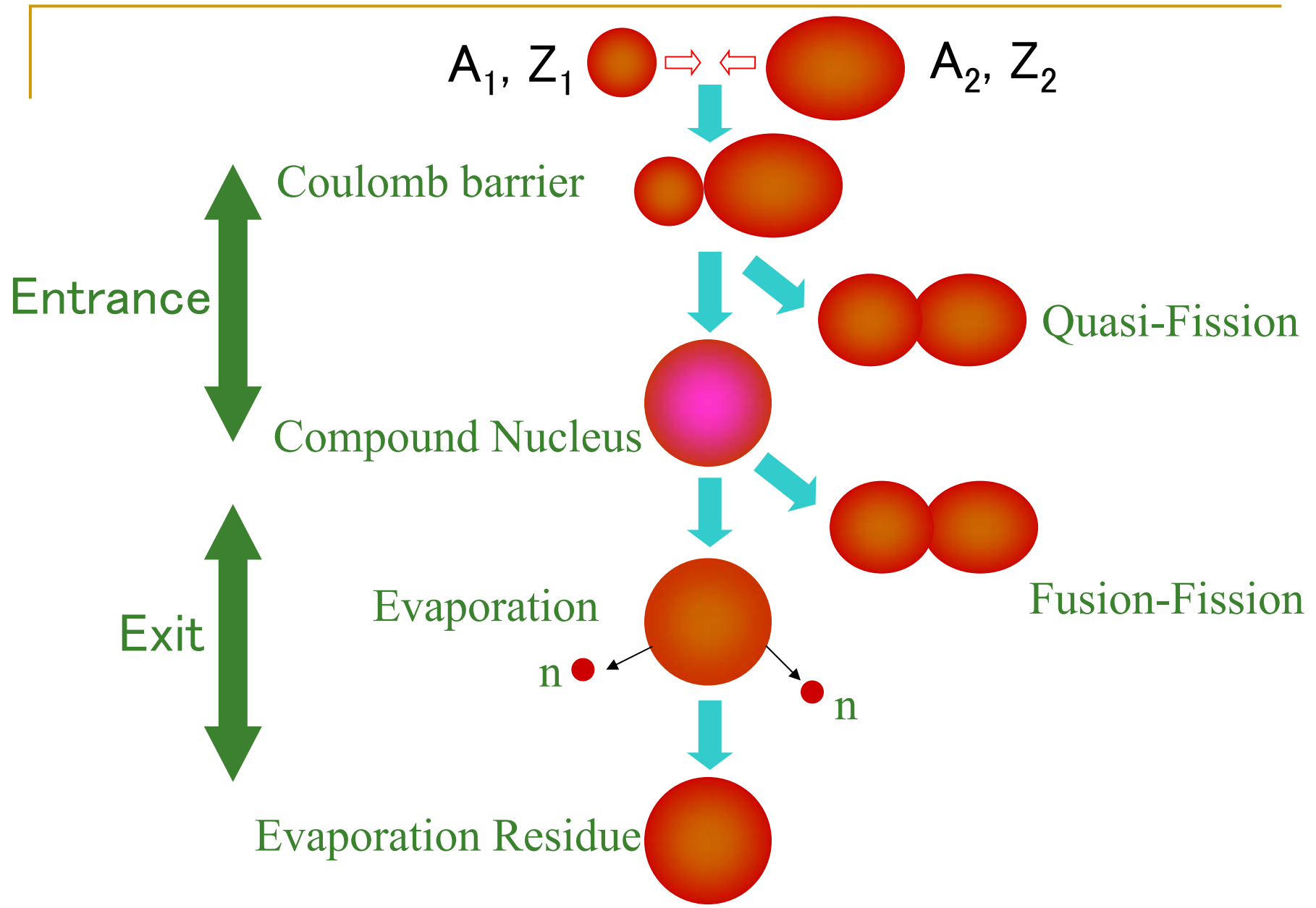
Independent deformation of fragments

Four-dimensional energy surface
elongation, 2 fragment deformations, mass-asymmetry



Superheavy Elements

- How many elements can exist in nature?
 - Stability against fission
 - Superheavy elements
 - Shell-stabilized : **No macroscopic fission barrier**
 - Heavy-ion fusion reaction
 - Hot fusion reaction
 - Actinide target + ^{48}Ca projectile
 - $E_{\text{ex}} = 30\text{-}40$ MeV
 - Cold fusion reaction
 - Pb, Bi target
 - $E_{\text{ex}} = 10\text{-}15$ MeV
-



Evaporation residue cross section

$$\sigma_{ER} = \pi \hat{\lambda}^2 \sum_l (2l + 1) T_l(E_{cm}) P_l^{for}(E_{cm}) P_l^{sur}(E^*)$$

- Evaporation residue cross section is extremely small in the synthesis of SHE

Picobarn = 10^{-12} barn

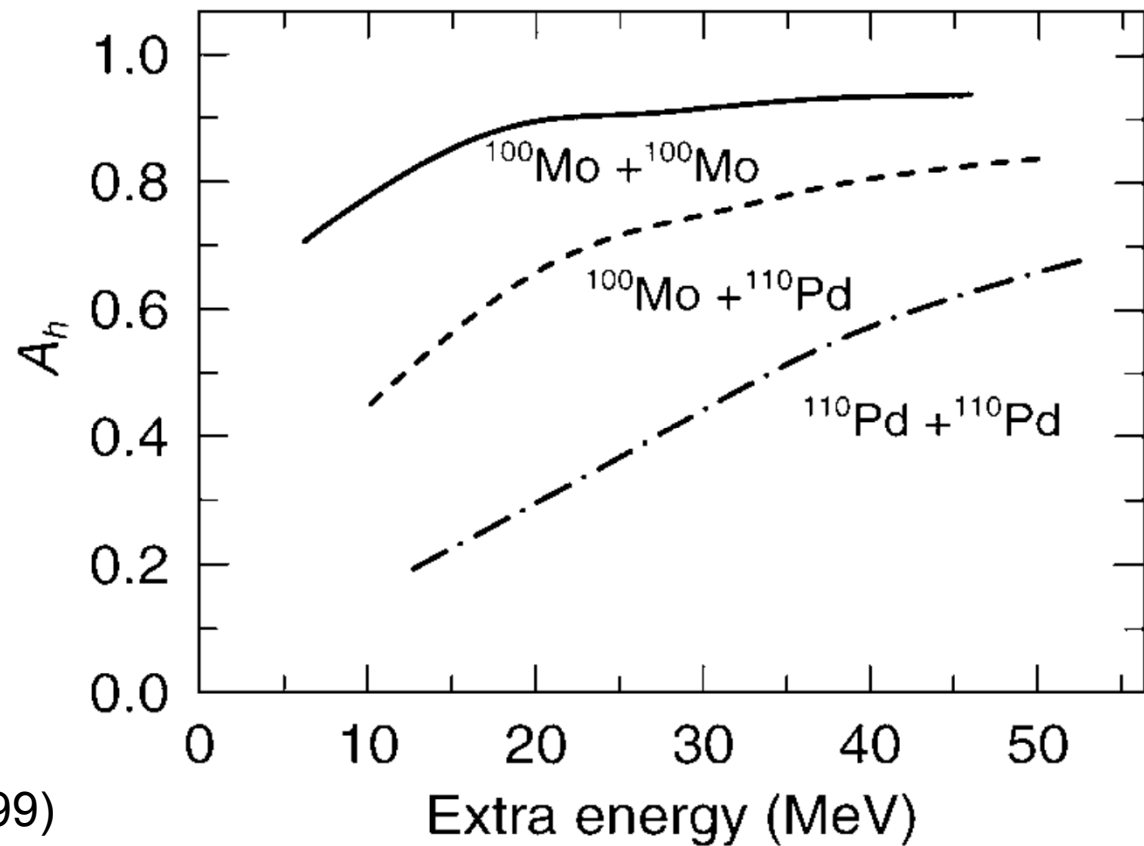
- T_l : sticking probability
 - Optical potential, dissipation
 - P_l^{for} : formation probability **small**
 - Fluctuation-dissipation dynamics
 - P_l^{sur} : survival probability **small**
 - Statistical approach
-

Fusion reaction of two heavy nuclei

- For lighter systems, fusion occurs when two nuclei touch each other.
 - For heavier systems, fusion does not always occur even when two nuclei touch.
 - Fusion hindrance
 - Extra fusion barrier inside the Coulomb barrier of the entrance channel.
 - For the synthesis of SHE, the fusion hindrance plays an essential roll.
 - Fusion probability by Langevin approach
-

Fusion hindrance

- Extra energy is necessary for fusion
 - Two-dimensional Langevin calculation
 - $Z_1 \times Z_2 > 1600$
 - Dissipation of relative motion



Fusion hindrance (one-dimensional model)

$$U = U_B - \frac{1}{2} m \omega_B^2 q^2 \quad \text{Parabolic barrier}$$

■ Formation probability

$$P^{for} = \frac{1}{2} \operatorname{erfc} \left[\left(\frac{aB^2}{K-B} \right)^{1/4} \sqrt{\frac{\beta + \beta'}{2\beta}} \left(1 - \frac{2\omega_B}{\beta + \beta'} \sqrt{\frac{K}{B}} \right) \right]$$

B : extra barrier height

K : extra kinetic energy (at contact)

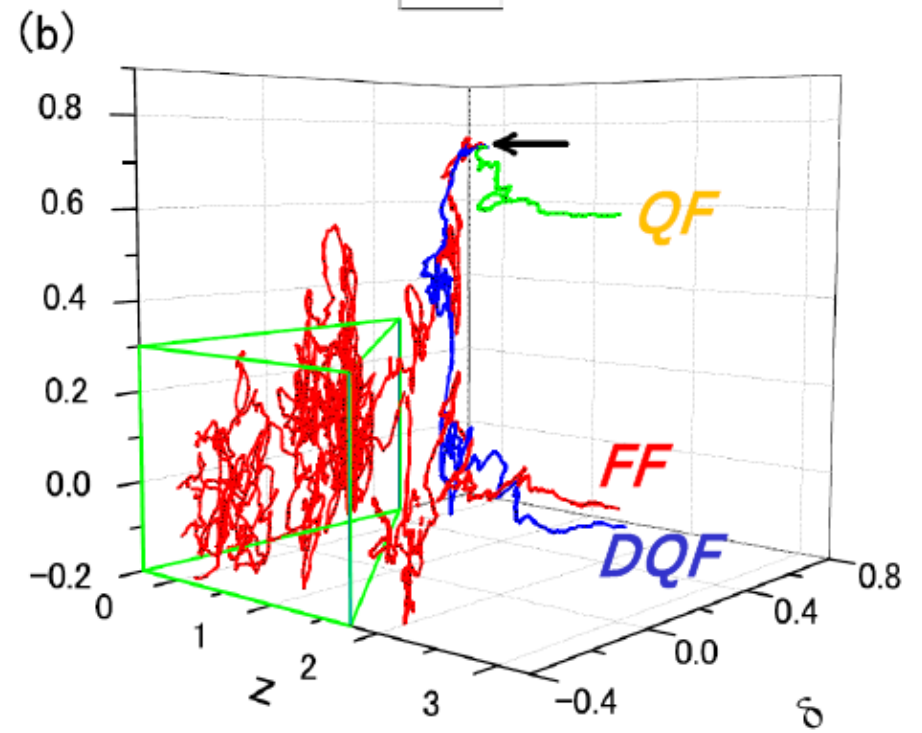
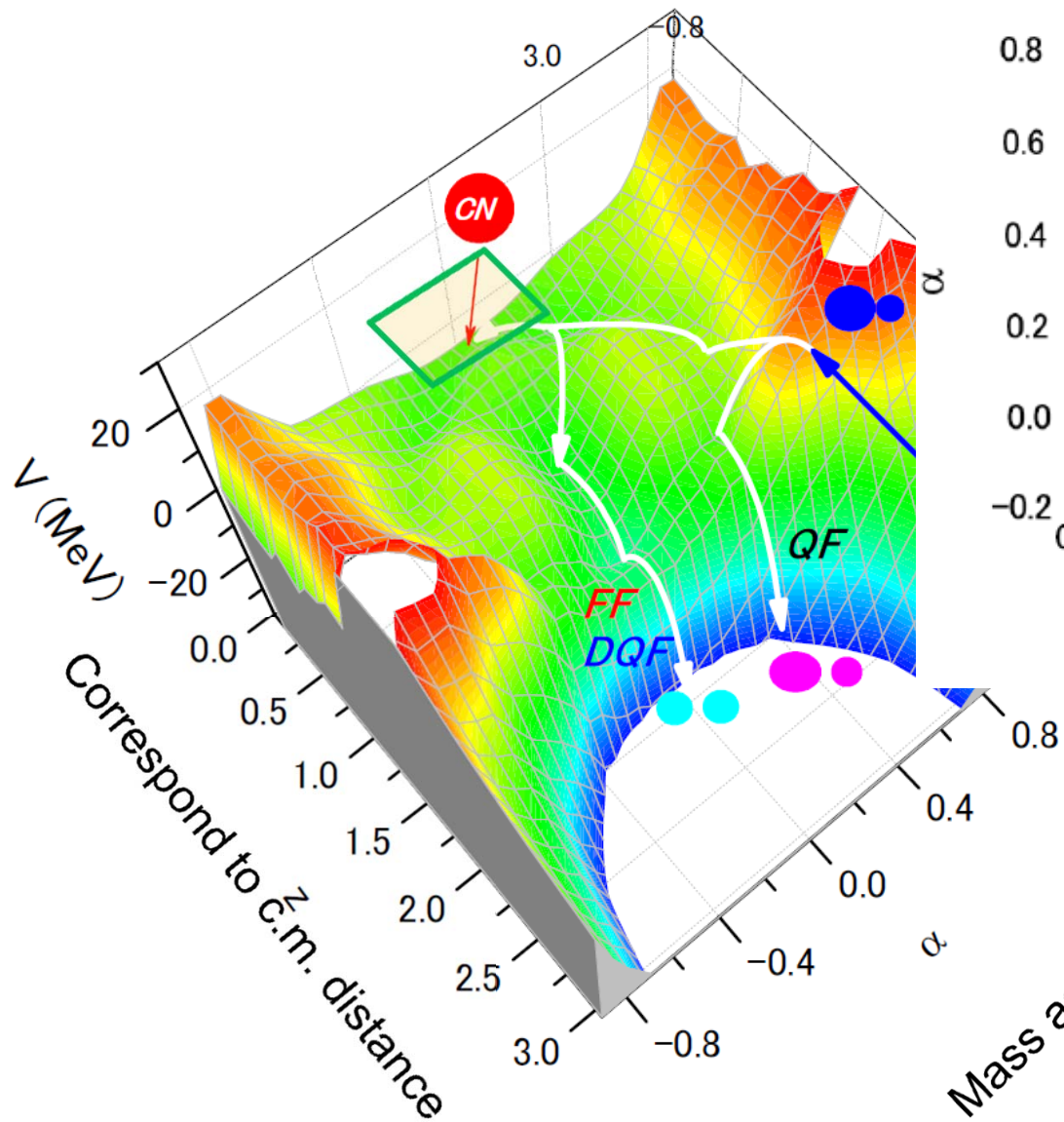
a : level density parameter

β : reduced friction parameter

■ Strong friction case

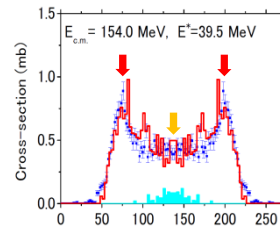
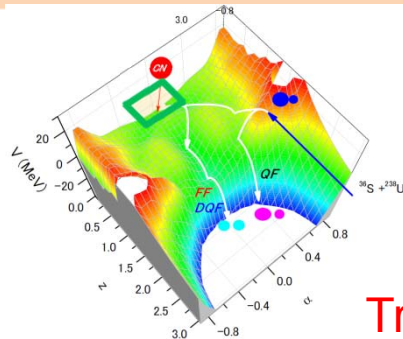
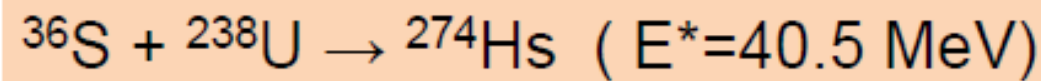
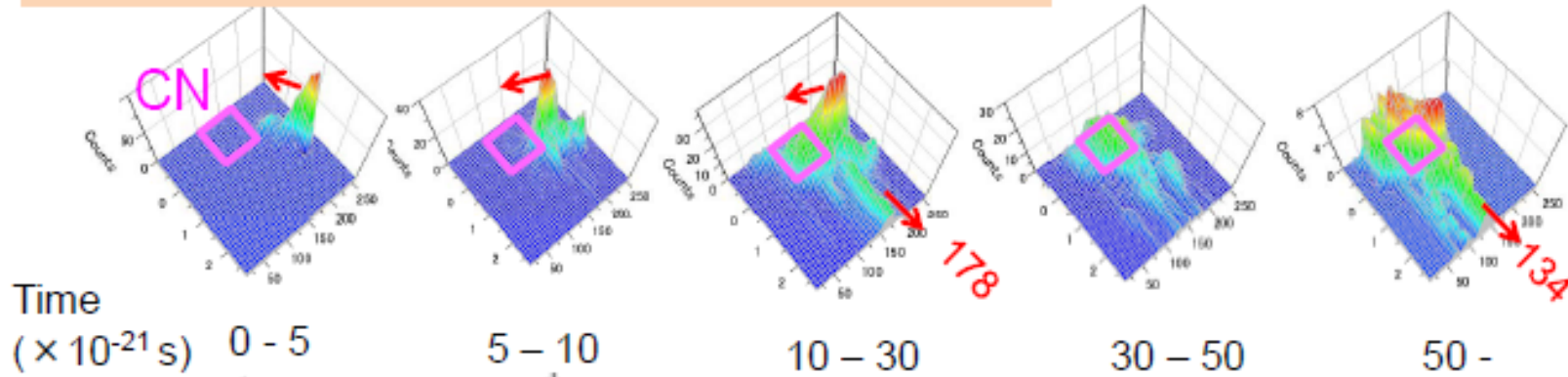
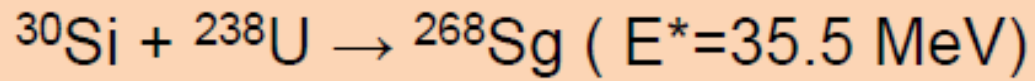
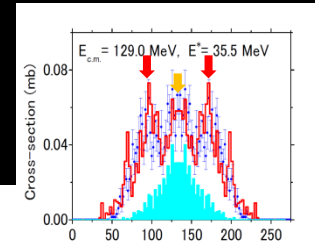
$$P^{for} = \frac{1}{2} \operatorname{erfc} \left[\left(\frac{aB^2}{K-B} \right)^{1/4} \left(1 - \frac{\omega_B}{\beta} \sqrt{\frac{K}{B}} \right) \right] \quad \beta' = \sqrt{\beta^2 + 4\omega_B^2}$$

Overview of Dynamical Process in reaction $^{36}\text{S}+^{238}\text{U}$



Mass asymmetry

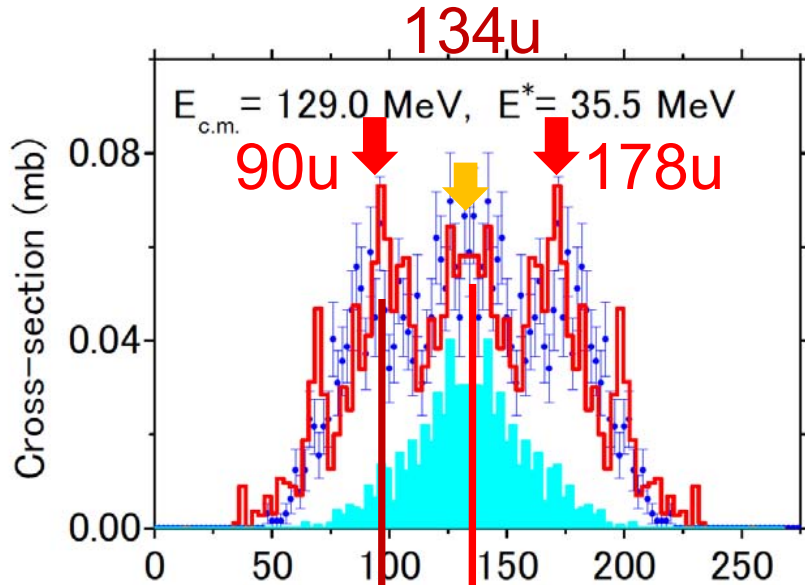
Time evolution of probability distribution



Mass Asymmetry; α
 Charge Center Distance; Z

Try to clarify the origin of difference between the both cases →

$^{30}\text{Si} + ^{238}\text{U}$

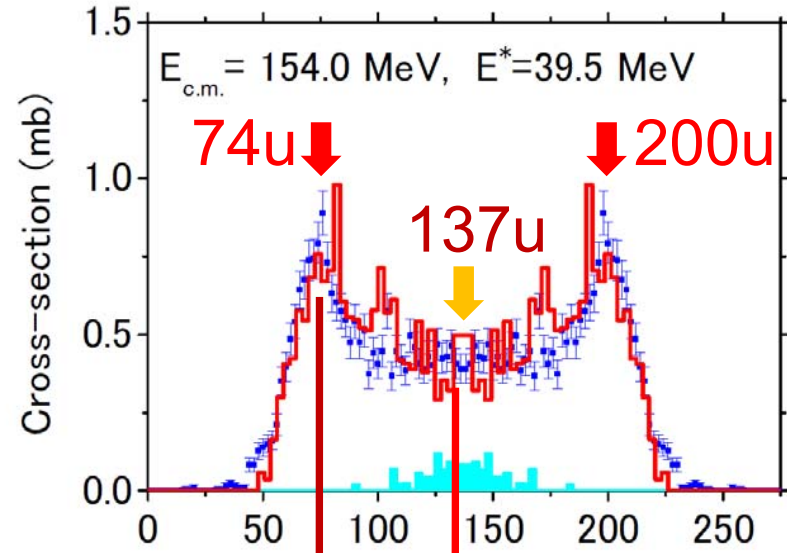


FF and DQF
 $t > 50 \times 10^{-21} \text{ sec}$
 $-0.2 < \delta < 0.2$ (peak 0)

QF via mono-nucleus
 $t < 30 \times 10^{-21} \text{ sec}$
 $0.2 < \delta < 0.5$ (peak 0.4)

- (1) Origin of reaction process
- (2) Building times
- (3) Deformation of fragments

$^{36}\text{S} + ^{238}\text{U}$



FF and DQF
 $t < 30 \times 10^{-21} \text{ sec}$
 $0 < \delta < 0.4$ (peak 0.2)

QF
 $t < 10 \times 10^{-21} \text{ sec}$
 $0 < \delta < 0.2$ (peak 0)

Summary

- The fluctuation-dissipation dynamics is a general framework to describe the dynamics of a few slow (collective) variables interacting with many fast variables that can be treated as a heat bath.
 - Powerful tool to study fission and heavy-ion fusion
 - Fission
 - Time scale of fission
 - Fragment mass and TKE distributions
 - Heavy-ion fusion reaction
 - Fusion hindrance
 - Quasi-fission and fusion-fission and more
-