X-ray optics for axion physics

Vistas in Axion Physics

25 April 2012



Michael Pivovaroff, PhD Group Leader, X-ray Science & Technology

This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under contract DE-AC52-07NA27344. Lawrence Livermore National Security, LLC

UCRL-PRES-550292





Acknowledgements

<u>LLNL</u>

Jennifer Alameda

Sherry Baker

Bill Craig

Todd Decker

Monica Fernandez-Perea

Paul Mirkarimi

Jeff Robinson

Regina Soufli

Julia Vogel

<u>DTU-Space</u>

Finn Christensen

Nicolai Brejnholt

Carsten Cooper-Jensen*

Anders Jakobsen



Fiona Harrison

Kristin Madsen

Peter Mao

ORNL Klaus Ziock

Columbia U.

Charles Hailey

Jason Koglin *

NASA GSFC Will Zhang

* Moved institutions

X-RAY OPTICS PRIMER



X-ray optics rely on a wide range of phenomena

Diffraction

- Gratings
- Fresnel zone plates





A Snigirev et al. *Nature*, **384**, 49, (1996)

Refraction

Compound refractive lens

Reflection

- Capillary optics
- Mirrors Today's talk

Absorption

- Pinholes
- Anger cameras
- Coded apertures

Reflective x-ray optics

- Compton first discovered X-rays incident at small glancing angles are totally reflected
 - "The Total Reflexion of X-rays", Philosophical Magazine, 45, 1121, (1923)
- Index of refraction for high energy photons $n = 1 \delta i\beta$
- Total external reflection of light occurs when the incident angle is less than the critical angle $\theta_{\rm C} = \sqrt{2\delta} \propto \sqrt{Z} / E$.
- Critical angle drops rapidly with energy $\theta_c \sim E^{-1}$.



Original reflective x-ray optic concepts

"Formation of Optical Images by X-rays" P Kirkpatrick, AV Baez J Opt Soc Amer, 38, 766, (1948)

"Spiegelsysteme streifenden Einfalls als abbildende Optiken für Röntgenstrahlen" H Wolter, *Phys Ann* 10, 94, (1952)



FIG. 11. Arrangement of concave mirrors to produce real images of extended objects with incidence at small grazing angles.

- Two (or more) concave, spherical mirrors
- Does not meet the Abbe sine rule



- Even number of conic surfaces of revolutions (hyperbola+parabola, hyperbola+ellipse, etc.)
- Nearly satisfies Abbe sine rule
- Significant increase in solid angle (compared to KB)

Wolter optics for x-ray astronomy

- Wolter originally proposed his designs for an x-ray microscope for biology
 - Not possible to fabricate in the 1950s
- Idea later adopted by Giacconi *et al.* for astronomy
 - Nobel prize in 2002



 Key innovation was the realization that mirrors could be nested inside one another to increase collecting area (solid angle)

X-ray reflectivity

Limited to materials that:

- can be polished well or deposited smoothly (*e.g.*, Ni, Rh, Au, Ir)
- (ideally) do not have absorption edges in operational band





 Reflectivity depends not only on material, but also its highspatial frequency roughness (*i.e.*, finish)

Multilayer performance

- Recipes can be tuned for application; tremendous versatility
- Systems can consist of 1000's of bilayers to just a few layers ("overcoatings")
- Practically, limited by absorption, stress, absorption, material properties and other constraints (cost, time)





- Semi-infinite Pt coating with $\sigma=3\text{\AA}$
- Constant-d: Pt/SiC, σ=3.0Å, N=90, d=35Å Γ=0.56
- Graded-d: Pt/SiC, σ=4.5 Å, N=566

X-ray multilayers

- At high energies, graze angles (θ_c) become too shallow for efficient optics: switch to multilayers
- Alternating layers of high- and low-Z materials act as reflecting interfaces, following Bragg's law

$$m\lambda = 2d\sin\theta \sqrt{1 - \frac{2\overline{\delta}}{\sin^2\theta}}.$$

- Theory described in 1920s-1930s
- First proposed for X-ray applications in early 1970s by Spiller *et al.*
- Initially, constant-d designs used for high reflectivity for particular bands



Later, Christensen *et al.* proposed [*Proc SPIE*, **1736**, 229, (1992)] varying *d*, to satisfy the Bragg equation over a range of *θ* and *λ*(~1/E) at high energies.

TELESCOPES FOR RECENT ASTROPHYSICS MISSIONS

Moving from the soft x-ray band ...

XMM-Newton; ESA

- 15" HPD
- 3 telescopes, 58 nested shells
- 120 m² surface area
- Mirrors: 200M DM (\$120M US)
- Total: \$700MUS
- Replicated from precision mandrels

Chandra; NASA

- 0.5" HPD
- 1 telescope, 4 nested shells
- 10 m² surface area
- Mirrors: \$700M US
- Total:\$1600M US
- Polished monolithic blanks

XMM telescope View </t

Chandra Zerodur substrate



NuSTAR, a NASA SMEX satellite scheduled for launch in June 2012



... into the hard x-ray band

XMM-Newton; ESA

- 15" HPD
- 3 telescopes, 58 nested shells
- 120 m² surface area
- Mirrors: 200M DM (\$120MUS)
- Total: \$700MUS
- Replicated from precision mandrels

Chandra; NASA

- 0.5" HPD
- 1 telescope, 4 nested shells
- 10 m² surface area
- Mirrors: \$700M US
- Total:\$1600M US
- Polished monolithic blanks







- 45" HPD goal
- 2 telescopes, 130 nested shells
- 80 m² surface area
- Mirrors: \$10-15M US
- Total: \$100MUS
- Thermally-formed, multilayer-coated mirrors

Solution: glass substrates

- Work dates back as far as 1988
 - Labov, *Applied Optics*, **27**, 1465, (1988).
- Columbia/DTU/LLNL starts in earnest in late 1990's for the High Energy Focusing Telescope (HEFT) balloon mission
- Start with flat panel float glass (Schott and Corning) which has nice thickness uniformity and excellent surface finish (roughness σ = few Å)
- Thermally form ("slump") into near net shape
 - Take flat pieces of glass and turn into cylindrical shapes
- Coat with appropriate reflective coatings
- Assemble into an optic

Optics assembly procedure

- Epoxy graphite spacers onto a mandrel and machined to the correct radius & angle (#1)
- Epoxy ML-coated substrates to spacers (#2)
- After epoxy cures, epoxy next layer of spacers to previous layer of glass (#3)
- Machine these spacers, epoxy another layer of glass into place (#4)
- Repeat until entire optic is assembled



J.E. Koglin *et a*l., *Proc. SPIE*, **4851**, 607, (2003)



Optics start with thermally forming substrates

- Optics PI, Charles Hailey, Columbia University
- Team includes: Columbia U., DTU-Space, NASA GSFC, LLNL





Substrate forming in oven

- GSFC approach slumps glass directly onto highly polished mandrels
- Excellent figure (10–20" HPD) has been demonstrated

Depth-graded multilayer coatings provide broad band response High throughput

- Two material systems used, driven by need to detect Ti-44 lines at 68 & 78 keV
 - Pt/C provides highest response
 - W/Si less expensive and smoother
- 10 different multilayer recipes used
- X-ray testing to optimize coatings and understand performance
 - 8 keV (DTU)
 - 60 keV (NSLS)
 - 🔹 10-90 keV (RaMCaF)
- Extensive metrology to validate models
 - Surface roughness, TEM compositional studies

High throughput magnetron sputtering chamber

Danish Technical University-Space Coating Facility

F Christensen et al., Proc SPIE, 8147, (2011)

Pivovaroff : 25 April 2012 LLNL-P

С

NuSTAR telescopes assembled at the Nevis Laboratories, Columbia University



Two custom-built assembly machines are used to precisely mount the glass segments at Columbia's Nevis Laboratory

> J Koglin *et al., Proc SPIE*, **8147,** (2011) W Craig *et al., Proc SPIE*, **8147,** (2011)



Glass is positioned and clamped for overnight cure of epoxy

Optic with more than 100 layers

NuSTAR telescope details

Focal Length	10.15 m	
Shell Radii	51–191 mm	2000
Graze Angles	0.074–0.224°	
Shell Length	225 mm	
Mirror Thickness	0.2 mm	
Shells Per Module	130	
Mirror Segments Per Module	2340	
C Hailey et al. Proc SPIE , 7732 , (2010)		
Outer Cover Graphite Spacers Support Koglin et al. Proc. SPIE. 8147. (2011)		
W Craig et al., Proc SPIE, 8147 , (2011)		

X-RAY OPTICS FOR SOLAR AXION PHYSICS



Guiding philosophy for an axion experiment $g_{a\gamma}^{4} \propto b^{1/2} \varepsilon^{-1} \times s^{1/2} \varepsilon_{0}^{-1} \times (BL)^{-2} A^{-1} \times t^{-1/2}$ detectors optics magnet exposure

B = magnetic field

L = magnet length

A = cross-sectional area
Optics are needed, primarily, because detectors have non-zero backgrounds (s above)

 ε_{o} = efficiency

b = background *s* = spot size

- Optics "squeeze" x-ray beam from a size equal to the diameter of the magnet bore to something much smaller
- Spectral response and effective area are also important (*E*, above)
 - Both of these properties influence the throughput of the optic
- Practical constrains
 - Size (e.g. focal length), cost

 $\varepsilon = efficiency$

t = time

Wolter basics



- Usually, start with maximum allowable graze angle α
- Next, use constraints (e.g., *f* < 1.6m for CAST or minimum allowable substrate radius ρ_{min})

How small can you go?

- Optics are usually specified in terms of angular resolution
- The source may also have angular extent
- State-of-the-possible today
 - Optics: 10-60 arcsec half-power diameter (HPD)
 - Sources: Solar axions come from the central 180" of the Sun
- CAST, ABRIXAS x-ray telescope
 - Spot size
 - 180"×f = 0.87 mrad × 1600 mm = 1.4 mm diameter (theory) = 3.4 mm diameter (actual)
 - CAST Magnet bore = 43 mm diameter
 - Reduction in area =(43/3.4)² ≈ 150



M. Kuster et al., New J. Phys, 9, 169, (2007)

Considerations for IAXO

- 8 magnet bores → at least this many telescopes
- Large areas, ρ = 300 mm
 - Cannot be asymmetric (like CAST)
- Need NuSTAR-like approach to fabrication to keep costs down
- Notional focal length
 - α_{max} ≈ 0.8°
 - $f_{\min} \approx \rho_{\max}/tan(4\alpha_{\max}) \approx 5.4 \text{ m}$
- Complex trade required to optimize spot-size and spectrally-matched throughput



Obscuration due to substrate edge blocking light

Optimal coatings depends on several factors

- Must worry about total system throughput:
 - $d\Phi(E) \otimes QE(E) \otimes EffArea(E)$ (axion spectrum, detector efficiency and telescope area)
- Fix α = 0.7° and QE is unity from (a) 2-5 keV or (b) 1-10 keV
- Compare pure Ni and Pt coatings with a simple bi-layer, B₄C on W

(a) 2-5 keV

(b) 1-10 keV



Optimal coatings depends on several factors

- Must worry about total system throughput:
 - $d\Phi(E) \otimes QE(E) \otimes EffArea(E)$ (axion spectrum, detector efficiency and telescope area)
- Fix α = 0.7° and QE is unity from (a) 2-5 keV or (b) 1-10 keV
- Compare pure Ni and Pt coatings with a simple bi-layer, B₄C on W

(a) 2-5 keV

(b) 1-10 keV

